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IN RE APPLICATION OF: KIMIHIRO SAITO, ET AL.

SERIAL NO: 10/714,866

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FOR: OPTICAL PICKUP DEVICE, RECORDING  
AND REPRODUCING APPARATUS AND  
GAP DETECTION METHOD

GROUP ART UNIT: 2627

**FILING OF CERTIFIED ENGLISH TRANSLATION UNDER 37 CFR 1.52(d)**

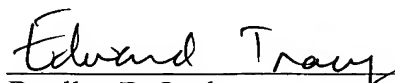
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SIR:

Applicants submit herewith a certified English translation of the Japanese priority document.

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AND GAP DETECTION METHOD ) PRIORITY DOCUMENT  
Honorable Commissioner of Patents  
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Washington, D.C. 20231

Sir:

I declare that I can read and speak both the English and Japanese languages, and that I have translated, fully and accurately, the following Japanese application(s) for which priority is claimed:

Copies of my English translation(s) of the above priority application(s) are attached hereto.

I further declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or document or any registration resulting therefrom.

Dated: November 14, 2006

By: Tadashi Shigeyama

Tadashi Shigeyama

[Title of Document] Specification

[Title of the Invention] OPTICAL PICKUP APPARATUS, RECORDING AND REPRODUCING APPARATUS AND GAP DETECTION METHOD

[Scope of Claim for a Patent]

[claim 1] In an optical pickup apparatus including a focusing lens with a numerical aperture greater than 1 composed of a solid immersion lens having a spherical surface portion and a flat surface portion parallel to the surface of an optical recording medium, a bundle of rays in a predetermined polarized state being irradiated on said optical recording medium from a light source through said focusing lens and a polarized state component perpendicular to the polarized state of reflected light obtained when a distance between the surface of said optical recording medium and the flat surface portion of said solid immersion lens is zero is detected from reflected light from said optical recording medium to obtain a signal corresponding to the distance between the surface of said optical recording medium and the flat surface portion of said solid immersion lens, an optical pickup apparatus characterized by comprising:

a beam splitter for reflecting both of a P-polarized light component and an S-polarized light component in reflected lights from said optical recording medium;

dividing means for dividing incident light into the P-polarized light component and the S-polarized light component reflected by said beam splitter; and

photo-detecting means for separately detecting the P-polarized light component and the S-polarized light component divided by said dividing means.

[claim 2] In an optical pickup apparatus according to claim 1, an optical pickup apparatus characterized in that said dividing means is a Wollaston prism.

[claim 3] In an optical pickup apparatus according to claim 1, an optical pickup apparatus characterized in that said dividing means is a Glan-Thompson prism.

[claim 4] In an optical pickup apparatus according to claim 1, an optical pickup apparatus characterized in that said dividing means is a polarizing and dividing grating.

[claim 5] In a recording and reproducing apparatus for recording and/or reproducing an optical recording medium by using an optical pickup apparatus including a focusing lens with a numerical aperture greater than 1 composed of a solid immersion lens having a spherical surface portion and a flat surface portion parallel to the surface of said optical recording medium, said optical pickup apparatus comprising a beam splitter for reflecting both of a P-polarized light component and an S-polarized light component in reflected lights from said optical recording medium, dividing means for dividing the P-polarized light component and the S-polarized light component reflected by said beam splitter and photo-detecting means for separately detecting the P-polarized light component and the S-polarized light component divided by said dividing means, a recording and

reproducing apparatus characterized by comprising:

drive means for adjusting a distance between said optical recording medium and said flat surface portion of said solid immersion lens; and

control means for controlling the adjustment state of said drive means based upon a detected signal obtained when light intensity of one polarized component detected by said photo-detecting means is detected as a signal corresponding to the distance between the surface of said optical recording medium and the flat surface portion of said solid immersion lens.

[claim 6] In a recording and reproducing apparatus according to claim 5, a recording and reproducing apparatus characterized by further comprising reproducing means for reproducing information from said optical recording medium based upon the other polarized light component detected by said photo-detecting means.

[claim 7] In a gap detection method for detecting a gap between a flat surface portion of a solid immersion lens and an optical recording medium by an optical pickup apparatus including a focusing lens with a numerical aperture greater than 1 composed of said solid immersion lens including a spherical surface portion and a flat surface portion parallel to the surface of said optical recording medium, when a bundle of rays in a predetermined polarized state is irradiated on the optical recording medium from a light source, a gap detection method characterized by comprising the steps of:

irradiating the optical recording medium with a bundle of

rays in a predetermined polarized state through the focusing lens;

reflecting both of a P-polarized light component and an S-polarized light component of reflected lights of a bundle of rays after the recording medium has been irradiated with a bundle of rays;

dividing the thus reflected P-polarized light component and S-polarized light component from each other; and

detecting a distance between the optical recording medium and the flat surface portion of the solid immersion lens based upon light intensity of any one polarized light component of the thus separated P-polarized light component and S-polarized light component.

[ Detailed Description of the Invention]

[ 0001]

[ Technical Field Pertinent to the Invention]

The present invention relates to an optical pickup apparatus, an optical recording and reproducing apparatus including this optical pickup apparatus (this optical recording and reproducing apparatus contains a magneto-optical recording and reproducing apparatus) and a gap detection method, and more particularly to an optical pickup apparatus, an optical recording and reproducing apparatus and a gap detection method suitable for use with a so-called near-field optical recording and reproducing system for recording and/or reproducing an optical recording medium while a numerical aperture of an

optical lens is increased.

[ 0002]

[ Prior Art]

Optical recording mediums, which are typically represented by a compact disc (CD), a mini disc (MD) and a digital video disc (DVD), have been so far widely used as storage mediums for storing therein music information, video information, data, programs and the like (optical recording medium in this specification includes a magneto-optical recording medium).

[ 0003]

These optical recording mediums can be recorded and/or reproduced by laser light irradiated on the signal recording surface of the medium from the optical pickup apparatus. More specifically, when the optical recording medium is reproduced by an optical pickup apparatus according to the related art, for example, very small changes of reflectance are read out from pits formed on one side of the optical recording medium through a non-contact objective lens, which is not in contact with the optical recording medium, such as an objective lens of a microscope and also, in the magneto-optical detection, miniscule magnetic domains are read out from the magneto-optical disc by a Kerr rotation angle.

[ 0004]

A size of a beam spot on the optical disc is roughly given by  $\lambda/NA$  (where  $\lambda$  is the wavelength of illumination light and NA is the numerical aperture of the lens), and resolution also is

proportional to this value. Here, with respect to the NA, the following equation is established:

[ 0005]

$$NA = n \cdot \sin\theta$$

(where n is the refractive index of the medium and  $\theta$  is the angle of marginal rays of light of the objective lens).

[ 0006]

When the medium is air, the NA is inhibited from exceeding 1. As a technology that can surpass this limit, there is proposed an optical pickup apparatus of a near-field optical recording and reproducing system which uses "solid immersion lens (Solid immersion lens) (see Non-Patent Document 1).

[ 0007]

This "solid immersion lens" has the same refractive index as that of an optical disc substrate and it is shaped like a part of a sphere including a spherical surface portion and a flat surface portion, the flat surface portion thereof being very close to the surface of the optical recording medium. Evanescent wave transmits through the boundary surface between the solid immersion lens and the optical disc, and this evanescent wave reaches the signal recording surface of the optical disc.

[ 0008]

[ Non-Patent Document 1]

Ichimura et. al, "Near-Field Phase-Change Optical Recording of 1.36 Numerical Aperture." Jpn. J. Appl. Phys. Vol. 39, 962-



967 (2000)

[ 0009]

[ Problem to be solved by the Invention]

Since it is customary for the above-mentioned optical pickup apparatus to read an information signal from the optical disc while the optical disc is being rotated, the optical disc and the solid immersion lens have to require a gap (space) therebetween. Accordingly, the evanescent wave should be used in order to achieve the NA greater than 1. The evanescent wave attenuates exponentially from the interface. Accordingly, the gap between the optical disc and the solid immersion lens should be made as extremely thin as about  $10/1$  of the wavelength  $\lambda$  of light from the light source of the optical pickup apparatus, for example and also, in order to reduce the area, the gap has to approach the signal recording surface.

[ 0010]

As a method for controlling such gap, there has hitherto been proposed a method for servo-controlling a distance between a solid immersion lens and an optical disc based upon an error signal after the gap error signal has been obtained by detecting an electrostatic capacity between an electrode formed on the surface of the solid immersion lens and the optical disc.

[ 0011]

However, in order to execute this method, the electrode has to be formed on the surface of the solid immersion lens and a signal line has to be led from this electrode to a control

circuit so that the apparatus becomes complex in arrangement, and hence it becomes difficult to manufacture the optical pickup apparatus.

[ 0012]

On the other hand, in the mastering process of the optical disc, the applicant of the present application has previously proposed a method for using returned light detected from a glass master disc as a gap error signal (see Japanese patent application No. H10-249880).

[ 0013]

When the solid immersion lens and the glass master disc have no gap therebetween, the surface of the solid immersion lens is in contact with the transparent photoresist on the glass master disc, and hence no light is returned from the surface of the solid immersion lens and conversely, when the solid immersion lens and the glass master disc have the gap therebetween, light that has been totally reflected on the surface of the solid immersion lens is returned, and the above previously-proposed method is able to detect the gap between the solid immersion lens and the glass master disc by using this light.

[ 0014]

However, this method can be used only when the master disc is made of glass and the photoresist for use in exposure is transparent and if the master disc has a reflective film such as an aluminum film, a phase-change film and a magneto-optical

recording film deposited on its surface like an optical disc, then even when the solid immersion lens and the master disc have no gap therebetween, light is reflected on the surface of the optical disc and no light is returned. Hence, this method may not be used.

[ 0015]

In order to solve the above-mentioned problem, the applicant of the present application has previously proposed an optical pickup apparatus that can accurately detect a very small gap between an optical disc with a reflective film deposited on its surface and a solid immersion lens (see Japanese patent application No. 2001-264467).

[ 0016]

This previously-proposed optical pickup apparatus will be described below with reference to the drawings and as shown in FIG. 8, the optical pickup apparatus includes an objective lens 2 composed of a solid immersion lens (SIL) 1 having a spherical portion and a flat surface portion parallel to the surface of an optical recording medium 90 to form a part of a shape of a sphere, the objective lens having a numerical aperture greater than 1. The solid immersion lens 1 is shaped like a hemisphere, for example, and it has a thickness substantially equal to the radius of the sphere. A distance (gap) between the flat surface portion of the solid immersion lens 1 and the surface of the optical recording medium 90 can be held at approximately  $10/1$  of the wavelength  $\lambda$  of light emitted from a semiconductor laser 3

serving as a light source under control of a servo mechanism which will be described later on.

[ 0017]

This optical pickup apparatus is able to obtain a gap error signal corresponding to a distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 1 by detecting a component of the polarized state perpendicular to the polarized state of reflected light obtained when a distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 1 is zero from reflected lights (returned lights) reflected on the optical recording medium 90 after they have been emitted from the semiconductor laser 3.

[ 0018]

Specifically, in this optical pickup apparatus, a bundle of rays emitted from the semiconductor laser 3 is collimated by a collimator lens 4 as a bundle of parallel rays and introduced into a beam splitter 5. A bundle of rays emitted from the semiconductor laser 3 has a wavelength of 400 nm, for example. A bundle of rays emitted from the semiconductor laser 3 transmits through the beam splitter 5 and becomes incident on a polarizing beam splitter 6. A bundle of rays emitted from the semiconductor laser 3 is a P-polarized light relative to the reflection surface of the polarizing beam splitter 6, and hence it transmits through the reflection surface and transmits through the polarizing beam splitter 6.

[ 0019]

A bundle of rays that has transmitted through the polarizing beam splitter 6 transmits through a  $[\lambda/4]$  (quarter-wave) plate 7 with its crystallographic axis inclined at an inclination angle of  $45^\circ$  relative to the direction of the incident polarized light, by which it is double-refracted so as to become circularly polarized light and the circularly polarized light is introduced into an objective lens 8 which configures the focusing lens 2 together with the solid immersion lens 1, and a bundle of incident parallel rays is converged by this objective lens 8 and introduced into the solid immersion lens 1. This objective lens 8 converges a bundle of parallel rays and introduces a bundle of parallel ray into the solid immersion lens 1. This solid immersion lens 1 has a focal point formed near a parallel portion disposed parallelly close to the surface of the optical recording medium 90. A refractive index of this solid immersion lens 1 is selected to be 1.8, for example.

[ 0020]

A bundle of the thus converged rays is focused on the signal recording surface of the optical recording medium 90 as evanescent wave. The objective lens 2 of this case has an NA (numerical aperture) of approximately 1.36, for example.

[ 0021]

The optical pickup apparatus shown in FIG. 8 is configured as the optical pickup apparatus capable of reproducing either an

optical disc on which an information signal is recorded by recording pits (concavities and convexities) or a recordable optical disc on which an information signal is recorded by using phase-change. More specifically, a bundle of rays that has been focused on the signal recording surface of the optical recording medium is reflected in various manners with or without application of the recording pits on this signal recording surface and returned to the polarizing beam splitter 6 through the objective lens 2 and the  $[\lambda/4]$  plate 7.

[ 0022]

A bundle of rays returned to the side of the focusing lens 2 after it has been reflected on the surface of the optical recording medium is introduced into the  $[\lambda/4]$  plate 7, in which it is changed in the form of circularly polarized light to linearly polarized light. At that time, the direction of polarized light is normal to the direction of polarization of a bundle of rays emitted from the semiconductor laser 3. Accordingly, a bundle of rays returned after it has been reflected on the optical recording medium is S-polarized light relative to the reflection surface of the polarizing beam splitter 6 and thereby reflected on this reflection surface so that it is deviated from the light path along which it may be returned to the semiconductor laser 3, thereby being received at a first detector 9 which is used to obtain a reproduced signal from the optical recording medium.

[ 0023]

In this optical pickup apparatus, on the surface A between the beam splitter 5 and the polarizing beam splitter 6, a bundle of rays emitted from the semiconductor laser 3 is linearly polarized light containing only an electric field component of X direction as shown in FIG. 9A but which does not contain an electric field component of Y direction as shown in FIG. 9B.

[ 0024]

Then, in the state in which the flat surface portion of the solid immersion lens 1 is in close contact with the surface of the optical recording medium 90, this flat surface portion is in close contact with a phase-change recording and reproducing multilayer film formed on the surface of the optical recording medium 90 as shown in FIG. 10A or a reflective film made of aluminum or the like formed on the surface of the optical recording medium 90 as shown in FIG. 10B.

[ 0025]

As described above, in the state in which the flat surface portion of the solid immersion lens 1 is in close contact with the surface of the optical recording medium 90, most of reflected light is inwardly and outwardly transmitted through the  $[\lambda/4]$  plate 7 and thereby the reflected light is double-refracted so as to have the direction of polarization rotated  $90^\circ$  so that a bundle of rays with a distribution substantially equal to that of light emitted from the semiconductor laser 3 may become incident on the surface B that is the surface just ahead of the first detector 9 as shown in FIG. 11A. At that time,

as shown in FIG. 11B, reflected light is hardly returned from the optical recording medium 90 to the surface A between the beam splitter 5 and the polarizing beam splitter 6.

[ 0026]

Then, in the state in which the solid immersion lens 1 is distant from the optical recording medium 90, as shown in FIG. 12, of light beams converged near the flat surface portion of the solid immersion lens 1, a light beam that will become incident on the flat surface portion at an incidence angle greater than a critical angle in this flat surface portion is reflected on the flat surface portion ((refractive index of solid immersion lens)  $\times$  sin (incidence angle)  $> 1$ ).

[ 0027]

In the thus reflected light, its direction of polarization is rotated delicately when it is totally reflected. Then, the light beam that has been totally reflected as described above contains a polarized light component perpendicular to the reflected light obtained in the state in which the flat surface portion of the solid immersion lens 1 is in close contact with the surface of the optical recording medium 90 as described above. As a result, a distribution of the returned light on the surface A between the beam splitter 5 and the polarizing beam splitter 6 becomes a distribution in which only light beams at the portions corresponding to the marginal portions of a bundle of rays are returned as shown in FIG. 13A.

[ 0028]



The light beam that has returned to the surface A as described above is reflected on the reflection surface of the beam splitter 5 and received at a second detector 10 which is used to obtain a gap error signal as shown in FIG. 8. This gap error signal is a signal corresponding to a distance between the flat surface portion of the solid immersion lens 1 and the optical recording medium 90.

[ 0029]

Then, at that time, a distribution of the returned light beam on the surface B located just ahead of the first detector 9 becomes a distribution in which returned light beams at the portions corresponding to the marginal portions of a bundle of rays are lost.

[ 0030]

In a relationship between a quantity of light received at the second detector 10 and the distance (air gap) between the flat surface portion of the solid immersion lens 1 and the surface of the optical recording medium 90, this distance (air gap) can be held at  $10/1$  of the wavelength by controlling the position at which the solid immersion lens 1 comes in contact with or comes away from the optical recording medium 90 in such a manner that the quantity of light at the second detector 10, for example, may be kept at the ratio of quantity of incident light of 0.2 as shown in FIG. 14.

[ 0031]

It should be noted that when the optical recording medium

90 is a magneto-optical disc, an optical pickup apparatus having an arrangement shown in FIG. 15, for example, can be applied to this example. Specifically, as shown in FIG. 15, a bundle of rays emitted from the semiconductor laser 3 is focused on the signal recording surface of the optical recording medium 90 through the collimator lens 4, the polarizing beam splitter 6, the beam splitter 5, the focusing lens 8 and the solid immersion lens 1. In this optical pickup apparatus, a  $[\lambda/4]$  plate is not provided on the outward light path to the optical recording medium 90.

[ 0032]

Then, the returned light that has been reflected on the optical recording medium 90 is divided by the beam splitter 5, whereafter it is refracted by a  $[\lambda/2]$  (half-wave) plate (polarization filter) 11 so that its direction of polarization is rotated  $45^\circ$  and introduced into a second polarizing beam splitter 12. This  $[\lambda/2]$  plate 11 is disposed with its optical axis inclined  $22.5^\circ$  relative to the direction of incident linearly polarized light.

[ 0033]

The light that became incident on the second polarizing beam splitter 12 is divided in response to a Kerr rotation angle generated based on a magneto-optical effect when it is reflected on the signal recording surface of the optical recording medium 90, and it is received at the first and second detectors 13 and 14, both of which are used to obtain a magneto-optical signal. A

difference signal between the outputted signals from the first and second detectors 13, 14 is not generated when a bundle of reflected rays does not generate the Kerr rotation angle and becomes an output corresponding to the Kerr rotation angle generated in a bundle of reflected rays, which becomes a magneto-optical signal.

[ 0034]

Then, a bundle of rays that has returned from the flat surface portion of the solid immersion lens 1 in order to obtain the gap error signal is returned through the beam splitter 5 to the polarizing beam splitter 6, reflected by this polarizing beam splitter 6 and received at the third detector 10 that is used to obtain the gap error signal.

[ 0035]

Also, when the optical recording medium 90 is the magneto-optical disc, the optical pickup apparatus may be modified as an optical pickup apparatus having an arrangement shown in FIG. 16, for example. Specifically, as shown in FIG. 16, a bundle of rays emitted from the semiconductor laser 3 may be focused on the signal recording surface of the optical recording medium 90 through the collimator lens 4, the beam splitter 5, the focusing lens 8 and the solid immersion lens 1.

[ 0036]

The light beam that has been irradiated on the signal recording surface of the optical recording medium 90 in this manner is reflected on this signal recording surface and

reflected on the beam splitter 5, whereafter it is further divided by the second beam splitter 15 into two bundles of rays. A bundle of rays that has passed the second beam splitter 15 is transmitted through the  $[\lambda/2]$  plate 11 and thereby its direction of polarization is rotated  $45^\circ$ , whereafter it is introduced into the polarizing beam splitter 12. This  $[\lambda/2]$  plate 11 is located such that its optical axis is inclined at an inclination angle of  $22.5^\circ$  relative to the direction of incident linearly polarized light.

[ 0037]

The light that has been introduced into the polarizing beam splitter 12 is divided in response to the Kerr rotation angle generated by the magneto-optical effect when it is reflected on the signal recording surface of the optical recording medium 90 and received at the first and second detectors 13 and 14 which are used to obtain the magneto-optical signal. A difference signal between the outputted signals from the first and second detectors 13, 14 is not generated when a bundle of reflected rays does not have the Kerr rotation angle, and becomes an output corresponding to the Kerr rotation angle generated in this bundle of rays, which becomes a magneto-optical signal.

[ 0038]

On the other hand, a bundle of rays reflected by the second beam splitter 15 is introduced into the second polarizing beam splitter 16. Of this bundle of rays, a bundle of rays that has returned from the flat surface portion of the solid immersion

lens 1 in order to obtain the gap error signal is reflected by the second polarizing beam splitter 16 and received at the third detector 10 that is used to obtain the gap error signal.

[ 0039]

Also in the optical pickup apparatus shown in FIG. 16, similarly to the case of the optical system shown in FIG. 8, the polarized state of incident light introduced into the beam splitter 5 becomes linearly polarized light that contains only the electric field component of the X direction as shown in FIG. 9A but that does not contain the electric field component of the Y direction as shown in FIG. 9B. Each of the beam splitters 5, 15 transmits and reflects the polarized components of both X, Y directions equally.

[ 0040]

When the flat surface portion of the solid immersion lens 1 is in close contact with the surface of the optical recording medium 90, this flat surface portion is in close contact with the phase-change recording and reproducing multilayer film formed on the surface of the optical recording medium 90 as shown in FIG. 17. A distribution of returned light on the surface B which is the surface required after the returned light has passed through the second polarizing beam splitter 16 at that time becomes a distribution substantially equal to those of lights emitted from the semiconductor laser 3 as shown in FIG. 18A. Then, in the surface C which is the surface disposed just before returned light is reflected by the second polarizing beam

splitter 16 and introduced into the third detector 10, the returned light from the optical recording medium 90 is hardly returned as shown in FIG. 18B. Accordingly, when the flat surface portion of the solid immersion lens 1 is in close contact with the surface of the optical recording medium 90, returned light on the surface C is almost zero, and hence returned light hardly reaches the third detector 10.

[ 0041]

Then, in the state in which the solid immersion lens 1 is distant from the optical recording medium 90, as shown in FIG. 12, of lights focused near the flat surface portion of the solid immersion lens 1, light incident on the flat surface portion at an angle exceeding the critical angle of this flat surface portion is totally reflected on this flat surface portion ( $(\text{refractive index of solid immersion lens}) \times \sin (\text{incidence angle}) > 1$ ).

[ 0042]

The thus totally reflected light delicately rotates its direction of polarization when it is totally reflected. Then, the thus totally reflected light contains a polarized component normal to the reflected light obtained in the state in which the flat surface portion of the solid immersion lens 1 is in close contact with the surface of the optical recording medium 90 as described above. As a result, a distribution of the returned light on the surface C which is the surface required just before the light is reflected by the second polarizing beam splitter 16

and introduced into the third detector 10 becomes a distribution in which the portions corresponding to the marginal portions of a bundle of rays are partly returned as shown in FIG. 19B.

[ 0043]

The light thus returned to the surface C is received at the second detector 10 which is used to obtain a gap error signal. This gap error signal is a signal corresponding to the distance between the flat surface portion of the solid immersion lens 1 and the surface of the optical recording medium 90.

[ 0044]

Then, at that time, a distribution of the returned light on the surface B which is the surface behind the second polarizing beam splitter 16 becomes a distribution in which the portions corresponding to the marginal portions of a bundle of rays are lost as shown in FIG. 19A.

[ 0045]

In a relationship between the quantity of light received at the third detector 10 and the distance (air gap) between the flat surface portion of the solid immersion lens 1 and the surface of the optical recording medium 90, as shown in FIG. 20, this distance (air gap) can be held at  $10/1$  of the wavelength of the light by controlling the position of the direction in which the solid immersion lens 1 comes in contact with or comes away from the optical recording medium 90 such that the quantity of light of the third detector 10, for example, is held at the ratio of quantity of incident light of 0.1.

[ 0046]

However, when these previously-proposed optical pickup apparatus are in use, the arrangement shown in FIG. 8 requires a plurality of beam splitters such as the beam splitter 5 for obtaining the gap error signal and the polarizing beam splitter 6 for obtaining the reproduced signal and also requires separately independent photo-detectors such as the detector 10 for obtaining the gap error signal and the detector 9 for obtaining the reproduced signal, and there arises a problem, in which the optical pickup apparatus becomes complex in arrangement. The optical pickup apparatus shown in FIGS. 15, 16 needs much more beam splitters and detectors. Also, a problem arises, in which the recording and reproducing apparatus requires the optical pickup apparatus having the complex arrangement so that the recording and reproducing apparatus which assembles such optical pickup apparatus also becomes complex in arrangement.

[ 0047]

In view of the aforesaid aspects, in this kind of near-field optical recording and reproducing system, a distance between a recording medium and a solid immersion lens can be detected and controlled with ease.

[.0048]

[ Means for solving the Problem]

An optical pickup apparatus according to the present invention is an optical pickup apparatus including a focusing



lens with a numerical aperture greater than 1 composed of a solid immersion lens having a spherical surface portion and a flat surface portion parallel to the surface of an optical recording medium, a bundle of rays in a predetermined polarized state being irradiated on the optical recording medium from a light source through the focusing lens and a polarized state component perpendicular to the polarized state of reflected light obtained when a distance between the surface of this optical recording medium and the flat surface portion of the solid immersion lens is zero is detected from reflected light from the optical recording medium to obtain a signal corresponding to the distance between the surface of the optical recording medium and the flat surface portion of the solid immersion lens, and there are included a beam splitter for reflecting both of a P-polarized light component and an S-polarized light component in reflected light beams from the optical recording medium, a dividing device for dividing the P-polarized light component and the S-polarized light component reflected by the beam splitter and a photo-detecting device for separately detecting the P-polarized light component and the S-polarized light component divided by the dividing device.

[ 0049]

Also, a recording and reproducing apparatus according to the present invention is a recording and reproducing apparatus for recording and/or reproducing an optical recording medium by using an optical pickup apparatus including a focusing lens with

a numerical aperture greater than 1 composed of a solid immersion lens having a spherical surface portion and a flat surface portion parallel to the surface of the optical recording medium, the optical pickup apparatus including a beam splitter for reflecting both of a P-polarized light component and an S-polarized light component in reflected light beams from the optical recording medium, a dividing device for dividing the P-polarized light component and the S-polarized light component reflected by the beam splitter and a photo-detecting device for separately detecting the P-polarized light component and the S-polarized light component divided by the dividing device, and there are included a drive device for adjusting a distance between the optical recording medium and the flat surface portion of the solid immersion lens and a control device for controlling the adjustment state of the drive device based upon a detected signal obtained when light intensity of one polarized component detected by the photo-detecting means is detected as a signal corresponding to the distance between the surface of the optical recording medium and the flat surface portion of the solid immersion lens.

[ 0050].

Also, a gap detection method according to the present invention is a gap detection method for detecting a gap between a flat surface portion of a solid immersion lens and an optical recording medium by an optical pickup apparatus including a focusing lens with a numerical aperture greater than 1 composed

of the solid immersion lens having a spherical surface portion and a flat surface portion parallel to the surface of the optical recording medium, when a bundle of rays in a predetermined polarized state is irradiated on the optical recording medium from a light source, and there are included the steps of irradiating the optical recording medium with a bundle of rays in a predetermined polarized state through the focusing lens, reflecting both of a P-polarized light component and an S-polarized light component of reflected light of the light beam after the light beam has irradiated the recording medium, dividing the thus reflected P-polarized light component and S-polarized light component and detecting a distance between the optical recording medium and the flat surface portion of the solid immersion lens based upon light intensity of any one polarized light component of the thus divided P-polarized light component and S-polarized light component.

[ 0051]

According to the present invention, since a beam splitter is provided to reflect both of a P-polarized light component and a S-polarized light component, the P-polarized light component and the S-polarized light component thus reflected by the beam splitter are divided and light intensity of one of the thus divided polarized light components is detected, it becomes possible to detect a signal corresponding to a distance between a flat surface portion of a solid immersion lens and the surface of an optical recording medium by a simple and efficient

arrangement.

[ 0052]

[Mode for Carrying Out the Invention]

Embodiments of the present invention will be described below, in which prior to the detailed description of the arrangement of the present invention, definitions of terms that are to be used in the following descriptions will be described, and in this specification, the term of an optical recording and reproducing apparatus refers to not only a recording and reproducing apparatus for recording and reproducing an optical recording medium but also a recording apparatus for recording an optical recording medium" and a "reproducing apparatus for reproducing an optical recording medium. Also, as has already been described, this optical recording medium also refers to other recording mediums such as a magneto-optical recording medium in and from which information can be recorded and reproduced optically.

[ 0053]

Next, a first embodiment of the present invention will be described with reference to FIGS. 1 and 2.

[ 0054]

FIGS. 1 are diagrams showing an arrangement of an optical pickup apparatus according to a first embodiment of the present invention. As shown in FIGS. 1, this optical pickup apparatus includes a semiconductor laser 101 prepared as a light source, and a bundle of rays from this semiconductor laser 101 is

introduced into a beam splitter 102. A bundle of rays emitted from the semiconductor laser 101 is transmitted through the beam splitter 102 and introduced into a  $[\lambda/4]$  (quarter-wave) plate 103. The  $[\lambda/4]$  plate 103 is disposed such that its crystallographic axis is inclined at an inclination angle of  $45^\circ$  relative to the direction of polarization of incident light. The incident light is emitted as circularly polarized light and this emitted light is introduced through a focusing lens composed of an objective lens 104 and a solid immersion lens (SIL) 105 into the signal recording surface of an optical recording medium 90.

[ 0055]

As has been so far described as the related-art technology, the solid immersion lens is disposed very close to the surface of the optical recording medium 90 (for example, about 50 nm) and it is of a so-called hemispherical lens in which one surface on the side close to the recording medium is shaped as a flat surface, the other surface close to the objective lens is shaped as a spherical surface, a thickness thereof being selected to be the same as the radius of the spherical surface. Alternatively, the solid immersion lens may be shaped like a super-hemispherical type lens having a thickness larger than the radius of the spherical surface configuring the lens. Also, with respect to the surface of the side close to the recording medium, only the central portion through which a bundle of rays of laser light is transmitted may be formed as a flat surface and the marginal portion around the central portion may be formed as a

suitable shape such as a cone. In the following description, the surface of the side close to the recording medium will be simply referred to as a flat surface, and herein, a flat surface refers to a flat surface in which a surface portion through which at least a bundle of rays of laser light is transmitted may be formed as a flat surface, and the whole of this surface portion need not always be shaped as the flat surface.

[ 0056]

As described above, when the objective lens 104 and the solid immersion lens 105 constitute the focusing lens, the numerical aperture (NA) of the focusing lens becomes greater than 1, and hence it becomes possible to record and reproduce information by the near-field optical recording and reproducing system.

[ 0057]

Light that has been reflected on the surface of the optical recording medium 90 is introduced through the solid immersion lens 105 and the objective lens 104 into the  $[\lambda/4]$  plate 103. Light passed through the  $[\lambda/4]$  plate 103 is refracted and thereby changed from circularly polarized light into linearly polarized light. The light that has transmitted through this  $[\lambda/4]$  plate 103 is introduced into the beam splitter 102. This beam splitter 102 is not a polarizing beam splitter but may be a beam splitter for polarizing a bundle of rays introduced thereto from the side of the optical recording medium 90 to provide two polarized light components of an S-polarized light component and

a P-polarized light component so that the two polarized light components may be reflected to the lateral direction. Specifically, in this beam splitter 102, its reflected light is given the same polarized light component as that of the light from the light source, and this beam splitter reflects 50% of the light incident thereon from the side of the objective lens 104, for example, to the lateral direction by the reflection surface thereof.

[ 0058]

The returned light that has been reflected to the lateral direction by the beam splitter 102 is introduced into a dividing means for dividing incident light into an S-polarized light component and a P-polarized light component. In this example, a Wollaston prism 110 is used as the dividing means, and the incident light is divided into an S-polarized light component and a P-polarized light component by the Wollaston prism 110, and the thus divided S-polarized light component and P-polarized light component are introduced into an RF signal detecting unit 121 and a gap error signal detecting unit 122 which are adjoining to each other on the same plane of the photo-detector 120.

[ 0059]

As shown in FIGS. 2, the Wollaston prism 110 is composed of a first prism 111 and a second prism 112 that are bonded to each other in such a manner that C axes of crystals of two prisms thereof may become different from each other  $90^\circ$ . When incident

light is refracted on a bonded surface 113 of the two prisms 111 and 112, light polarized in the same direction as the C-axis direction of the first prism 111 is given an emission angle  $\theta_0$  (incidence angle  $\theta_1$ ) that can satisfy  $n_1 \sin \theta_1 = n_2 \sin \theta_0$  on the bonded surface. Also, light polarized in the opposite direction of the C-axis direction of the first prism 111 is given the emission angle  $\theta_0$  that can satisfy  $n_2 \sin \theta_1 = n_1 \sin \theta_0$  on the bonded surface.

[ 0060]

Accordingly, the photo-detector 120 having the two adjacent photo-detecting units 121, 122 on the same plane is disposed at a light emission portion from which the light that has transmitted through this Wollaston prism 110 is emitted, whereby the S-polarized light component is introduced into the RF signal detecting unit 121 of the photo-detector 120 and the P-polarized light component is introduced into the gap error signal detecting unit 122 of the photo-detector 120. The signal introduced into the RF signal detecting unit 121 becomes a signal corresponding to concavities and convexities of the pits of the optical recording medium 90 so that information can be reproduced from the recording medium 90. The signal introduced into the gap error signal detecting unit 122 becomes a gap error signal of which the light intensity changes in response to the distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105.

[ 0061]



The P-polarized light component becomes the gap error signal based upon the same principle as that has already been referred to as the related-art technology. Specifically, by detecting a component of the polarized state perpendicular to the polarized state of reflected light obtained when the distance between the surface of the optical recording medium and the flat surface portion of the solid immersion lens is zero from the reflected light (returned light) that was reflected by the optical recording medium after they have been emitted from the semiconductor laser, it is possible to obtain the gap error signal corresponding to the distance between the surface of the optical recording medium and the flat surface portion of the solid immersion lens.

[ 0062]

By using the thus detected gap error signal, it becomes possible to servo-control the distance between the optical recording medium 90 and the solid immersion lens 105. A servo control mechanism will be described later on.

[ 0063]

With the arrangement shown in FIGS. 1 and FIGS. 2, since the S-polarized light component and the P-polarized light component of the reflected light from the optical recording medium 90 can separately be detected by the simple arrangement using one beam splitter 102 and the Wollaston prism 110 serving as the dividing means for dividing incident light into the S-polarized light component and the P-polarized light component,

the optical pickup apparatus can be simplified in arrangement as compared with the related-art optical pickup apparatus using a plurality of beam splitters, which can contribute to miniaturization of the optical pickup apparatus. Also, with respect to the photo-detector, it is sufficient to prepare one photo-detector 120 that can detect the two polarized light components emitted from the Wollaston prism 110 at the adjacent two photo-detection positions on the same plane, and hence the photo-detector can be simplified in arrangement as compared with the case in which a plurality of photo-detectors are separately located at the different positions like the related-art. Also, when the optical pickup apparatus according to this embodiment is attached to the optical recording and reproducing apparatus, the recording and reproducing apparatus can be simplified in arrangement and miniaturized in size.

[ 0064]

Next, a second embodiment of the present invention will be described with reference to FIGS. 3 and 4. In FIGS. 3 and FIG. 4, elements and parts identical to those of FIGS. 1 that have been referred to in the first embodiment are denoted by identical reference numerals.

[ 0065]

According to this embodiment, while the Wollaston prism is used as the dividing means for dividing the incident light into the P-polarized light component and the S-polarized light component in the first embodiment, this embodiment uses a Glan-

Thompson lens as the dividing means. A rest of the arrangement of the optical system is the same as that of the optical pickup apparatus that has been described in the first embodiment.

[ 0066]

Specifically, as shown in FIGS. 3, there is prepared the semiconductor laser 101 as the light source, and a bundle of rays from this semiconductor laser 101 is introduced into the beam splitter 102. A bundle of rays incident on the beam splitter from the semiconductor laser 101 is traveled through the beam splitter 102 and introduced into the  $[\lambda/4]$  (quarter-wave) plate 103. The  $[\lambda/4]$  plate 103 is disposed such that its crystallographic axis is inclined at an inclination angle of  $45^\circ$  relative to the direction of polarization of the incident light, and this quarter-wave plate refracts the incident light to provide circularly polarized light, and the light from the quarter-wave plate is introduced into the signal recording surface of the optical recording medium 90 through a focusing lens with a numerical aperture (NA) greater than 1 composed of the objective lens 104 and the solid immersion lens (SIL) 105.

[ 0067]

Light that has been reflected on the surface of the optical recording medium 90 is introduced through the solid immersion lens 105 and the objective lens 104 into the  $[\lambda/4]$  plate 103. The  $[\lambda/4]$  plate 103 refracts the incident light to change circularly polarized light to linearly polarized light. A bundle

of rays that has transmitted through the  $[\lambda/4]$  plate 103 is introduced into the beam splitter 102. The beam splitter 102 is not the polarizing beam splitter but may be a beam splitter for reflecting both of polarized light components of an S-polarized light component and a P-polarized light component of a bundle of rays introduced thereto from the side of the optical recording medium 90 to the lateral side.

[ 0068]

The returned light reflected to the lateral side by the beam splitter 102 is introduced into the dividing means that divides incident light into an S-polarized light component and a P-polarized light component. In this example, a Glan-Thompson prism 130 is used as the dividing means, the incident light is divided into an S-polarized light component and a P-polarized light component by the Glan-Thompson prism 130 and the thus divided S-polarized light component and P-polarized light component are introduced into an RF signal detecting unit 141 and a gap error signal detecting unit 142 which are adjacent to each other on the same plane of a photo-detector 140.

[ 0069]

The Glan-Thompson prism 130 is configured by bonding a glass 131 and a prism 132 together on a bonded surface 133 as shown in FIG. 4. When incident light is refracted on the bonded surface 133, polarized light polarized in the same direction as the C-axis direction of the prism 132 is given an emission angle  $\theta_0$  (incidence angle  $\theta_1$ ) that can satisfy  $n_0 \sin \theta_1 = n_1 \sin \theta_0$  on the

bonded surface. Also, light polarized in the opposite direction of the C-axis direction of the prism 132 is given an emission angle  $\theta_0$  that can satisfy  $n_0 \sin \theta_1 = n_2 \sin \theta_0$  on the bonded surface.

[ 0070]

Accordingly, the photo-detector 140 having the adjacent two photo-detecting units 141, 142 on the same plane is located at a light emission portion from which light that has transmitted through the Glan-Thompson prism 130 is emitted, whereby the S-polarized light component is introduced into the RF signal detecting unit 141 of the photo-detector 140 and the P-polarized light component is introduced into the gap error signal detecting unit 142 of the photo-detector 140. Since the Wollaston prism 110 that has been described in the first embodiment and the Glan-Thompson prism 130 have different emission angles of two polarized light components, the photo-detector 140 used in this embodiment has to locate its respective photo-detecting units at slightly different positions from those at which the photo-detector 120 that has been described in the first embodiment has located its respective photo-detecting units.

[ 0071]

With this arrangement, the signal that is introduced into the RF signal detecting unit 141 becomes a signal corresponding to concavities and convexities of the pits on the optical recording medium 90 so that information can be reproduced from the recording medium 90, and the signal that is introduced into

the gap error signal detecting unit 142 becomes a gap error signal of which the light intensity changes in response to the distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105, and by using this gap error signal, it becomes possible to servo-control the distance between the optical recording medium 90 and the solid immersion lens 105. Accordingly, similarly to the optical pickup apparatus that has been described so far in the first embodiment, also in this embodiment, the optical pickup apparatus can be simplified in arrangement and miniaturized in size, which can contribute to simplification and miniaturization of the recording and reproducing apparatus can be simplified.

[ 0072]

Next, a third embodiment of the present invention will be described with reference to FIGS. 3 and FIG. 4. In FIGS. 3 and FIG. 4, elements and parts identical to those of FIGS. 1 and FIGS. 3 that have been described in the first and second embodiments are denoted by identical reference numerals.

[ 0073]

In this embodiment, while the Wollaston prism or the Glan-Thompson prism was used as the dividing means for dividing incident light into the P-polarized light component and the S-polarized light component in the first and second embodiments, according to this embodiment, a polarizing and dividing grating is used as the dividing means. A rest of fundamental

arrangements of the optical system is the same as that of the arrangements of the optical pickup apparatus that have been described so far in the first and second embodiments.

[ 0074]

Specifically, as shown in FIGS. 5, the semiconductor laser 101 is prepared as the light source, and a bundle of rays from this semiconductor laser 101 is introduced into the beam splitter 102. A bundle of rays incident on the beam splitter 102 from the semiconductor laser 101 transmits through the beam splitter 102 and becomes incident on the  $[\lambda/4]$  (quarter-wave) plate 103. This  $[\lambda/4]$  plate 103 is disposed such that its crystallographic axis is inclined at an inclination angle of  $45^\circ$  relative to the direction of polarization of incident light. The quarter-wave plate refracts the incident light to provide circularly polarized light, and the emitted light from the quarter-wave plate is introduced into the signal recording surface of the optical recording medium 90 through the focusing lens with the numerical aperture (NA) greater than 1 composed of the objective lens 104 and the solid immersion lens (SIL) 105.

[ 0075]

Light reflected on the surface of the optical recording medium 90 is introduced into the  $[\lambda/4]$  plate 103 through the solid immersion lens 105 and the objective lens 104. The  $[\lambda/4]$  plate 103 refracts the circularly polarized light to provide linearly polarized light. A bundle of rays that has passed

through the  $[\lambda/4]$  plate 103 is introduced into the beam splitter 102. The beam splitter 102 is not a polarizing beam splitter but is a beam splitter for reflecting a bundle of rays incident thereon from the side of the optical recording medium 90 as two polarized light components of an S-polarized light component and a P-polarized light component to the lateral direction.

[ 0076]

The returned light that has been reflected toward the lateral side by the beam splitter 102 is introduced into a dividing means for dividing incident light into an S-polarized light component and a P-polarized light component. In this example, a polarizing and dividing grating 150 is used as the dividing means, and the incident light is divided into an S-polarized light component and a P-polarized light component by the polarizing and dividing grating 150, and the thus divided S-polarized light component and P-polarized light component are introduced into three photo-detecting units 161, 162, 163 adjacent on the same plane of a photo-detector 160. The P-polarized light component is divided into two polarized light components and the thus divided two polarized light components are introduced into the two photo-detecting units 161 and 163. The S-polarized light component is introduced into the photo-detecting unit 162.

[ 0077]

The polarizing and dividing grating 150 has a substrate



made of crystal such as  $\text{LiNbO}_3$  in which a hydrogen substituted region 151 with lithium (Li) substituted with hydrogen (H) is formed on the surface of the substrate like a grating, a refractive index of the region 151 being selected to be  $n_2$  regardless of the direction of polarization. Assuming that the thickness of the substituted region 151 is  $T$ , then with respect to the polarized light component of the C-axis direction, a phase difference of  $2\pi(n_1 - n_2)T/\lambda$  occurs between the substituted region 151 and other region and thereby the polarizing and dividing grating acts as a grating. On the other hand, with respect to the polarized light component of the direction opposite to the C-axis direction, a refractive index difference does not occur between the substituted region and other region, and hence incident light transmits through the polarizing and dividing grating 150 without being diffracted. Assuming that  $P$  is the pitch of the grating, then an angle  $\theta$  of the polarized component of the diffracted C-axis direction is given by  $\lambda/P = \sin\theta$ .

[ 0078]

Accordingly, the photo-detector 160 with the three photo-detecting units 161, 162, 163 adjacent on the same plane is located at a light emission portion from which light that has passed through this polarizing and dividing grating 150 is emitted, whereby the P-polarized light component is introduced into the two gap error signal detecting units 161 and 163 and a gap error signal is obtained by using any one of the signals

obtained at the two gap error signal detecting units 161, 163 or by using a signal which results from adding the two signals obtained from the two gap error signal detecting units 161, 163. This gap error signal has light intensity that changes in response to the distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105, and by using this gap error signal, it becomes possible to servo-control the distance between the optical recording medium 90 and the solid immersion lens 105 becomes possible.

[ 0079]

The S-polarized light component is introduced into the RF signal detecting unit 162 and the signal obtained at this RF signal detecting unit 162 becomes the signal corresponding to concavities and convexities of the pits on the optical recording medium 90 so that information can be reproduced from the recording medium 90. Accordingly, similarly to the optical pickup apparatus that have been described in the first and second embodiments, also in this embodiment, the optical pickup apparatus can be simplified in arrangement and miniaturized in size, which can contribute to simplification and miniaturization of the recording and reproducing apparatus.

[ 0080]

Next, an example of a servo mechanism for servo-controlling the position of the optical system when the optical recording and reproducing medium is recorded or reproduced with

application of the optical pickup apparatus of the above-mentioned respective embodiments will be described with reference to FIG. 7. When the optical recording medium such as an optical disc and a magneto-optical disc is recorded or reproduced by using the optical pickup apparatus, the positions of a lens and the like should be servo-controlled by using a servo mechanism. In particular, this example requires a servo mechanism by which a distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105 can be held at a predetermined distance. As shown in FIG. 7, this servo mechanism includes a coil 20 serving as a means for moving the solid immersion lens 105 in the direction perpendicular to the surface of the optical recording medium 90, a servo circuit 21 and a control circuit 22 serving as a control means for controlling this servo circuit 21. The servo circuit 21 is able to set the distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105 to the state instructed by the control circuit 22 in response to a signal applied to the coil 20.

[ 0081]

Then, the control circuit 22 supplies a command to the servo circuit 21 so as to maintain the light intensity of the gap error signal, detected by the gap error signal detecting unit 122 of the photo-detector 120 (in the case of the first embodiment), at predetermined light intensity, thereby

maintaining a constant distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105. It should be noted that, herein, the solid immersion lens 105 can be controlled in position in unison with the objective lens 104 by the coil 20.

[ 0082]

To maintain the light intensity detected by the detecting unit 122 at predetermined intensity, the output signal from the detecting unit 122, for example, is compared with a predetermined reference value. This reference value can be determined by the following first, second and third processing, for example.

[ 0083]

The first processing is such one that a mean value between an output value outputted from the gap error signal detecting unit when the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 1 are in close contact with each other (distance therebetween is zero) and an outputted value outputted from the gap error signal detecting unit when a distance between the surface and the flat surface portion is sufficiently large is set to a reference value. Also, in the second processing, a distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105 is measured, correlation between this measured value and the outputted value from the gap error signal detecting unit is calculated, whereafter an outputted value

corresponding to a predetermined distance is specified and set to a reference value. Further, the third processing is such one that  $1/2$  of the value outputted from the gap error signal detecting unit when the distance between the surface of the optical recording medium 90 and the flat surface portion of the solid immersion lens 105 is sufficiently large is set to a reference value. Any one of the first, second and third processing may be applied to the present invention.

[ 0084]

It should be noted that, as shown in FIG. 7, the output from the RF signal detecting unit (detecting unit 121 in the first embodiment) of the photo-detector (photo-detector 120 in the first embodiment) may be supplied to a reproducing block 24, in which it is processed by reproducing processing to thereby making it possible to reproduce information from the optical recording medium 90. Also, when information is recorded on the optical recording medium 90, record processing can be carried out by generating a drive signal for driving the semiconductor laser 101 (in the case of the recording medium in which information is recorded by using pits or phase-change) or a drive signal for driving a magnetic field modulation coil (in the case of a magneto-optical recording medium) based upon a signal that has been processed by a recording block 25. Also, the control circuit for carrying out servo control may servo-control a spindle motor 26 that rotates the optical recording medium 90.

[ 0085]

It should be noted that the present invention is not limited to the above-mentioned embodiments and that it may take various other arrangements without departing from the gist of the present invention. For example, as the dividing means for dividing the incident light into the P-polarized light wave and the S-polarized light wave, there can be used other dividing means than the Wollaston prism, the Glan-Thompson prism and the polarizing and dividing grating in the above-mentioned first, second and third embodiments. Even when the polarizing and dividing grating is in use, there can be used a polarizing and dividing grating composed of other crystal structure than the crystal structure that has been referred to in the above-mentioned embodiments. Also, the servo mechanism is not limited to the above-mentioned servo mechanism having the arrangement shown in FIG. 7 and it may be modified as a servo mechanism for driving a solid immersion lens and the like.

[ 0086]

[ Effect of the Invention]

According to the present invention, since the beam splitter reflects both of the P-polarized light component and the S-polarized light component, the P-polarized light component and the S-polarized light component reflected by this beam splitter are divided from each other and the light intensity of one of the divided polarized light component is detected, it becomes possible to detect the distance between the flat surface portion

of the solid immersion lens and the surface of the optical recording medium by the simple and efficient arrangement.

[ 0087]

In this case, since the Wollaston prism, the Glan-Thompson prism or the polarizing and dividing grating is used as the dividing means, for example, the P-polarized light component and the S-polarized light component can be divided from each other by the simple arrangement, and hence it becomes possible to individually detect the P-polarized light component and the S-polarized light component.

[ Brief Description of Drawings]

[ FIG. 1]

Diagrams showing an arrangement of an example of a main portion of an optical pickup apparatus according to a first embodiment of the present invention, wherein FIG. 1A is a side view of the optical pickup apparatus and FIG. 1B is a plan view of a pattern of a photo-detector;

[ FIG. 2]

Diagrams to which reference will be made in explaining a Wollaston prism that is applicable to the optical pickup apparatus according to the first embodiment of the present invention, wherein FIG. 2A is a diagram showing an arrangement of the Wollaston prism and FIG. 2B is a diagram showing polarization directions in the respective prisms;

[ FIG. 3]

Diagrams showing an example of a main portion of an

arrangement of an optical pickup apparatus according to a second embodiment of the present invention, wherein FIG. 3A is a side view of the optical pickup apparatus and FIG. 3B is a plan view showing a pattern of a photo-detector;

[ FIG. 4]

Diagrams to which reference will be made in explaining a Glan-Thompson prism which is applicable to the optical pickup apparatus according to the second embodiment of the present invention, wherein FIG. 4A is a diagram showing an arrangement of the Glan-Thompson prism and FIG. 4B is a diagram showing polarization directions of respective prisms;

[ FIG. 5]

Diagrams showing an arrangement of an example of a main portion of an optical pickup apparatus according to a third embodiment of the present invention, wherein FIG. 5A is a side view of the optical pickup apparatus and FIG. 5B is a plan view showing a pattern of a photo-detector;

[ FIG. 6]

Diagrams to which reference will be made in explaining a polarizing and dividing grating which is applicable to the optical pickup apparatus according to the third embodiment of the present invention, wherein FIG. 6A is a perspective view showing an arrangement of the polarizing and dividing grating, FIG. 6B is a diagram showing the polarization directions in the polarizing and dividing grating and FIG. 6C is a diagram showing a cross-section of the polarizing and dividing grating;



[ FIG. 7]

A block diagram showing an example of an arrangement of a servo system that is applicable to the respective embodiments of the present invention;

[ FIG. 8]

A side view showing an example of an arrangement of an optical pickup apparatus according to the related art;

[ FIG. 9]

An explanatory diagrams showing X component and Y component of an electric field of a bundle of rays incident on an optical recording medium in the optical pickup apparatus of the example of the related art shown in FIG. 8;

[ FIG. 10]

A longitudinal cross-sectional views showing the state in which a solid immersion lens in the optical pickup apparatus is in close contact with the optical recording medium;

[ FIG. 11]

An explanatory diagrams showing distributions of returned light returned from the optical recording medium when the solid immersion lens in the optical pickup apparatus is in close contact with the optical recording medium;

[ FIG. 12]

A longitudinal cross-sectional view showing the state in which the solid immersion lens in the optical pickup apparatus is distant from the optical recording medium;

[ FIG. 13]

An explanatory diagrams showing distributions of returned light returned from the optical recording medium when the solid immersion lens in the optical pickup apparatus is distant from the optical recording medium;

[ FIG. 14]

A diagram showing characteristic curves to which reference will be made in explaining an example of a relationship between a distance between the solid immersion lens in the optical pickup apparatus and the optical recording medium and a gap error signal;

[ FIG. 15]

A side view showing other example of an arrangement of an optical pickup apparatus according to the related art;

[ FIG. 16]

A side view showing a further example of an arrangement of an optical pickup apparatus according to the related art;

[ FIG. 17]

A longitudinal cross-sectional view showing the state in which a solid immersion lens in the optical pickup apparatus in the example shown in FIG. 16 is in close contact with the optical recording medium;

[ FIG. 18]

An explanatory diagrams showing distributions of light beams returned from the optical recording medium when the solid immersion lens in the optical pickup apparatus in the example shown in FIG. 16 is in close contact with the optical recording

medium;

[ FIG. 19]

An explanatory diagrams showing distributions of light beams returned from the optical recording medium when the solid immersion lens in the optical pickup apparatus in the example shown in FIG. 16 is distant from the optical recording medium; and

[ FIG. 20]

A diagram showing characteristic curves to which reference will be made in explaining a relationship between the distance between the solid immersion lens in the optical pickup apparatus in the example shown in FIG. 16 and the optical recording medium and a gap error signal;

[ Description of Reference Numerals]

1 ... solid immersion lens (SIL), 2 ... objective lens, 3 ... semiconductor laser, 4 ... collimator lens, 5, 15 ... beam splitter, 6, 12, 16 ... polarizing beam splitter, 7 ... [ $\lambda/4$ ] wave plate, 8 ... focusing lens, 9, 10, 13, 14 ... detector, 11 ... [ $\lambda/2$ ] plate, 20 ... coil, 21 ... servo circuit, 22 ... control circuit, 23 ... comparator, 24 ... reproducing block, 25 ... recording block, 26 ... spindle motor, 101 ... semiconductor laser, 102 ... beam splitter, 103 ... [ $\lambda/4$ ] wave plate, 104 ... objective lens, 105 ... solid immersion lens (SIL), 110 ... Wollaston prism, 111 ... first prism, 112 ... second prism, 120 ... detector, 121 ... RF signal detector,

122 ... gap error signal detecting unit, 130 ... Glan-Thompson  
prism, 131 ... glass portion, 132 ... prism, 140 ... detector, 121 ...  
RF signal detecting unit, 122 ... gap error signal detecting unit,  
150 ... polarizing and dividing grating, 151 ... hydrogen  
substituted region

[ Title of Document] Abstract

[ Abstract]

[ Problem] The present invention intends to obtain an optical pickup apparatus and an optical recording and reproducing apparatus suitable for use with a near-field optical recording and reproducing system.

[ Solving Means] An optical pickup apparatus includes an objective lens composed of a solid immersion lens (SIL), the objective lens having a numerical aperture greater than 1, a beam splitter 102 for reflecting both of a P-polarized light component and an S-polarized light component of reflected lights from an optical recording medium when the optical pickup apparatus irradiates the optical recording medium with a bundle of rays in a predetermined polarized state from a light source through the objective lens to detect a component in the polarized state perpendicular to the polarized state of reflected light obtained when a distance between the surface of this optical recording medium and the flat surface portion of the SIL is zero to produce a signal corresponding to the distance between the surface of the optical recording medium and the flat surface portion of the solid immersion lens, a dividing means 110 for dividing incident light into a P-polarized light component and an S-polarized light component reflected by the beam splitter and a photo-detecting means 120 for separately detecting the P-polarized light component and the S-polarized light component divided by the dividing means.

[ Selected Drawing] FIG. 1